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The Designated ' roject +ommittee Approves the ' roject Titled

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DE2E-3 ' E , T 3F A +UBESAT

By atthe* +t , apoli

The +u%eSat standard *as designed to provide quic(5 lo* cost access to space mainly for universities and research institutions. To further reduce the cost and improve the customi6a%ility of +u%eSats, polymer e7trusion additive manufacturing has %een proposed as a method for %uilding +u%eSat structures. A \$D8printed +u%eSat structure *as designed, %uilt and analy6ed to prove the concept of an e7trusion %ased additive manufacturing for small satellites. High outgassing from \$D8 printed ABS plastic could affect other launch payloads as *ell as any optics on the +u%eSat %ut other materials can %e su%stituted in its place. This project sho*s that additive manufacturing is a via%le method for +u%eSat production.

Figure 1A; 2015 Stresses Top 10 Bottom 10 B.....
Figure 1B; % Sat Specification Drawing.....
Figure 1C; % Sat Acceptance (list).....

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Currently, most CubeSat projects incorporate either specialized kits for their CubeSat structures or must custom build them from metal, usually aluminum. These options can be both costly and time consuming.

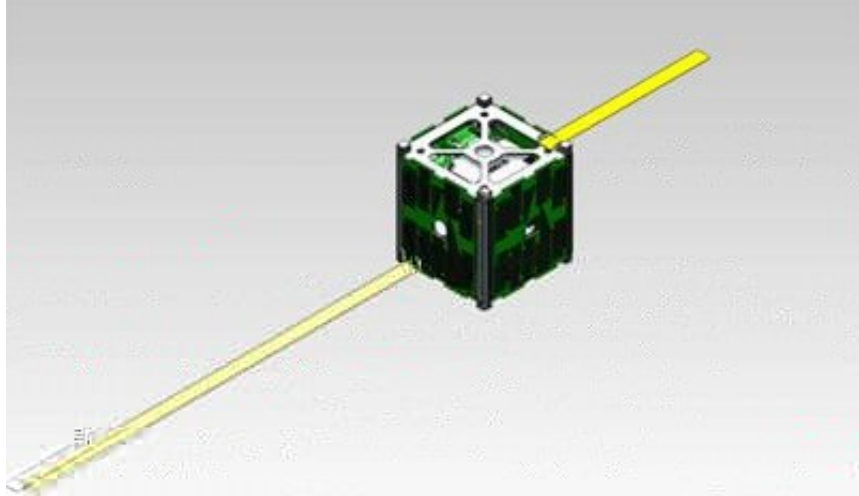


Figure #; TechEd Sat <Source; SJSU-

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The FDM printing process uses a spool of plastic which is melted and extruded through a nozzle. A head of material is deposited on a platform while the printer controls the horizontal placement. When one layer is complete the platform moves down and another layer is started. This process is continued with each layer adhering to the one below it as shown in Figure 1.

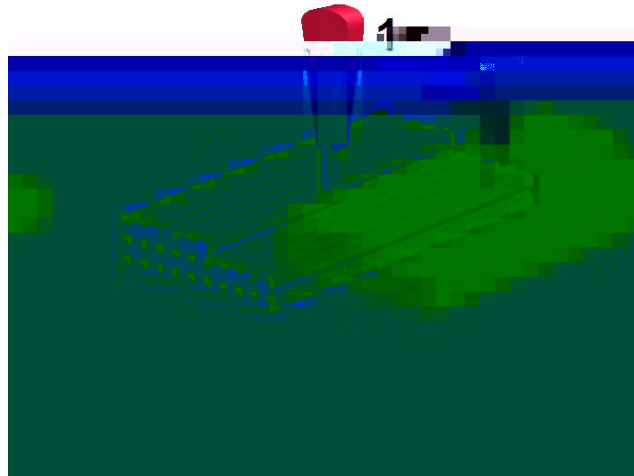


Figure 1; FDM layering

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Figure B; .A .T +u%eSat at 2arious Design Stages

Figure B above shows various iterations of the .A .T +u%eSat's structural design. This image displays two significant attributes of additive manufacturing. First, multiple iterations of the design are

fully optimize the structure. While their procedure for material testing can be utilized, unfortunately the material properties will need to be retested as they vary by printer model.

Additive manufacturing has been most often utilized as a method for rapid prototyping. In this sense, 3D printing has been used in numerous UAV projects. The prototypes can be used to visualize the design, sort out system integration issues, configure the components, or just be used as a model for display purposes. After the printed parts are created and the design has been set, the parts can then be manufactured out of traditional materials. Figure C below shows some examples of prototyped UAVs.



Figure C; 3D printed UAV prototypes, ASA

2.1

A 3D printed UAV was designed and analyzed to see if it meets the standard requirements for a UAV. There are several unknowns about 3D printing that needed to be addressed prior to design. A set of standard material properties of 3D printed ABS has not been universally accepted. Material testing will be performed to determine the strength of printed parts. Figure 2.1 shows the results of the material testing.

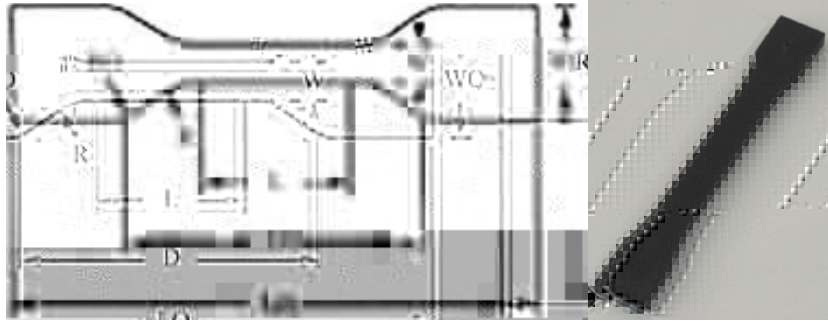


Figure D; ASTM D 5045 Dogbone Test Coupon 9A

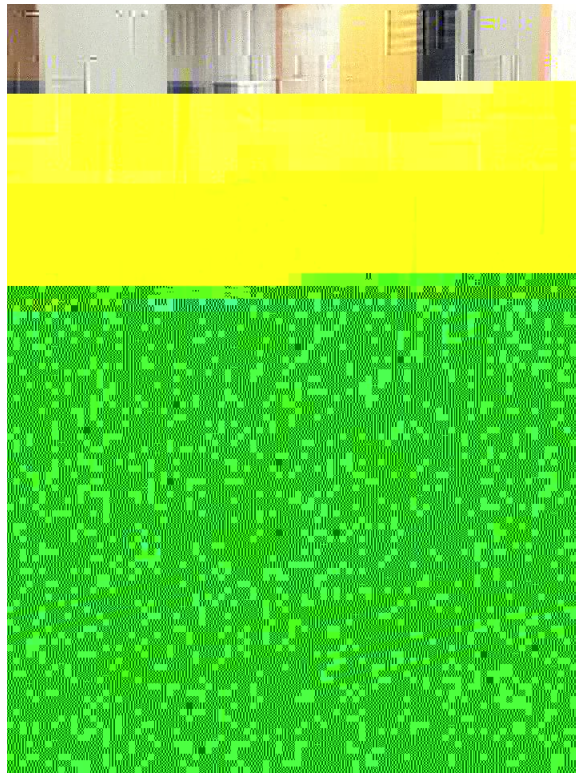


Figure E; Instron Universal Test Machine SJSU Materials Lab

Siemens dogbones *

ABS being the rating on the raw feedstock material prior to printing. Both the horizontal and vertical tests show the average of the samples tested.

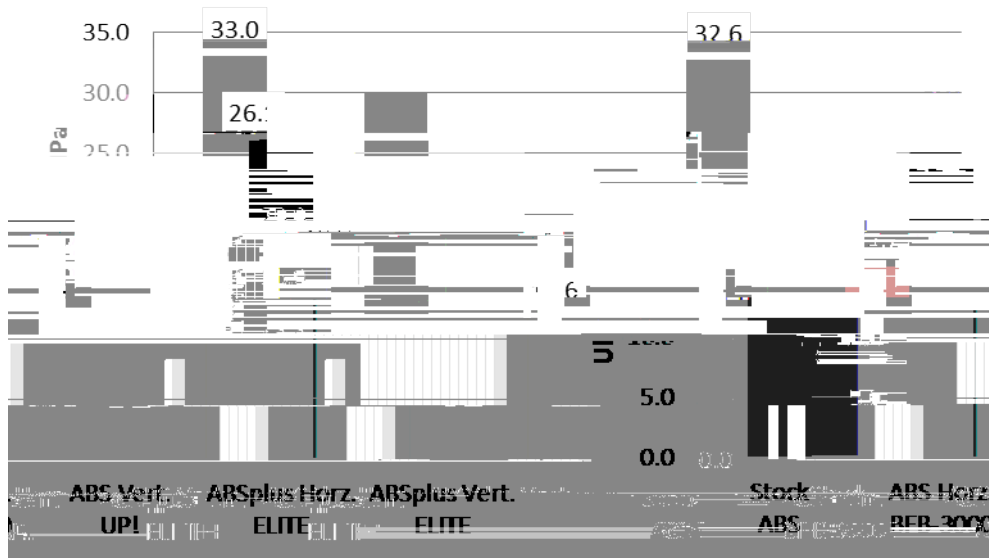
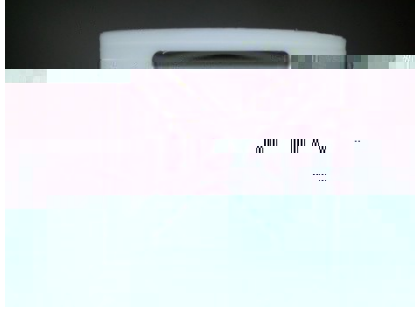
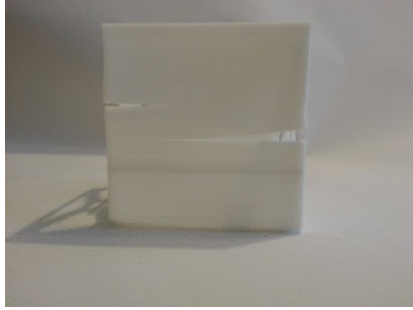
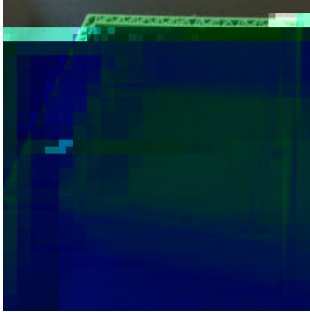


Figure 1: Tensile Strength of Solid Injection Molding

The ultimate tensile strength for solid injection molded ABS is rated at 35 MPa. Testing showed the strength of the adhesive bond (vertical tests) was significantly lower.





The preliminary 3D printed CubeSat design contains standard low cost off the shelf CubeSat components. The electrical power system (EES) flight module's transceivers and solar panels are catalog components from Amptron and Lyde Space. The structure is custom designed to be manufactured using an FDM printer.

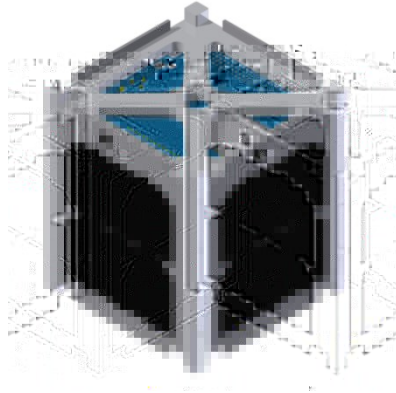


Figure #A; 3D printed CubeSat Design

The Amptron FBS Flight module is a single board computer for harsh environments. The module controls command and Data Handling (SD) communications (3-axis) mass storage and power switching. The board requires a C2 power input to power its 8-bit microcontroller, temperature sensors, clocks and 2/3. The module contains a 8-pin connector for stacking boards. A model of the FBS is shown in Figure #B.



Figure #B; Amptron FBS Flight module

The linear EES module from Amptron is a rechargeable electrical power system for CubeSat (its /t provides a regulated C2 and 2 power supply using two 1000mAh lithium batteries for a total of 20 Wh of power. The stackable design shown in Figure #C eliminates the need for additional wiring between boards. The module also interfaces with the Solar Array to recharge the batteries.

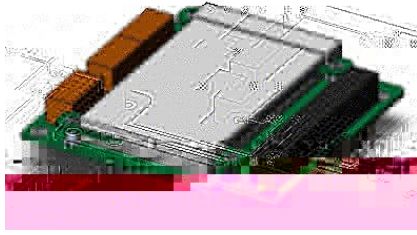


Figure #C; 'ump(in -inear E'S module

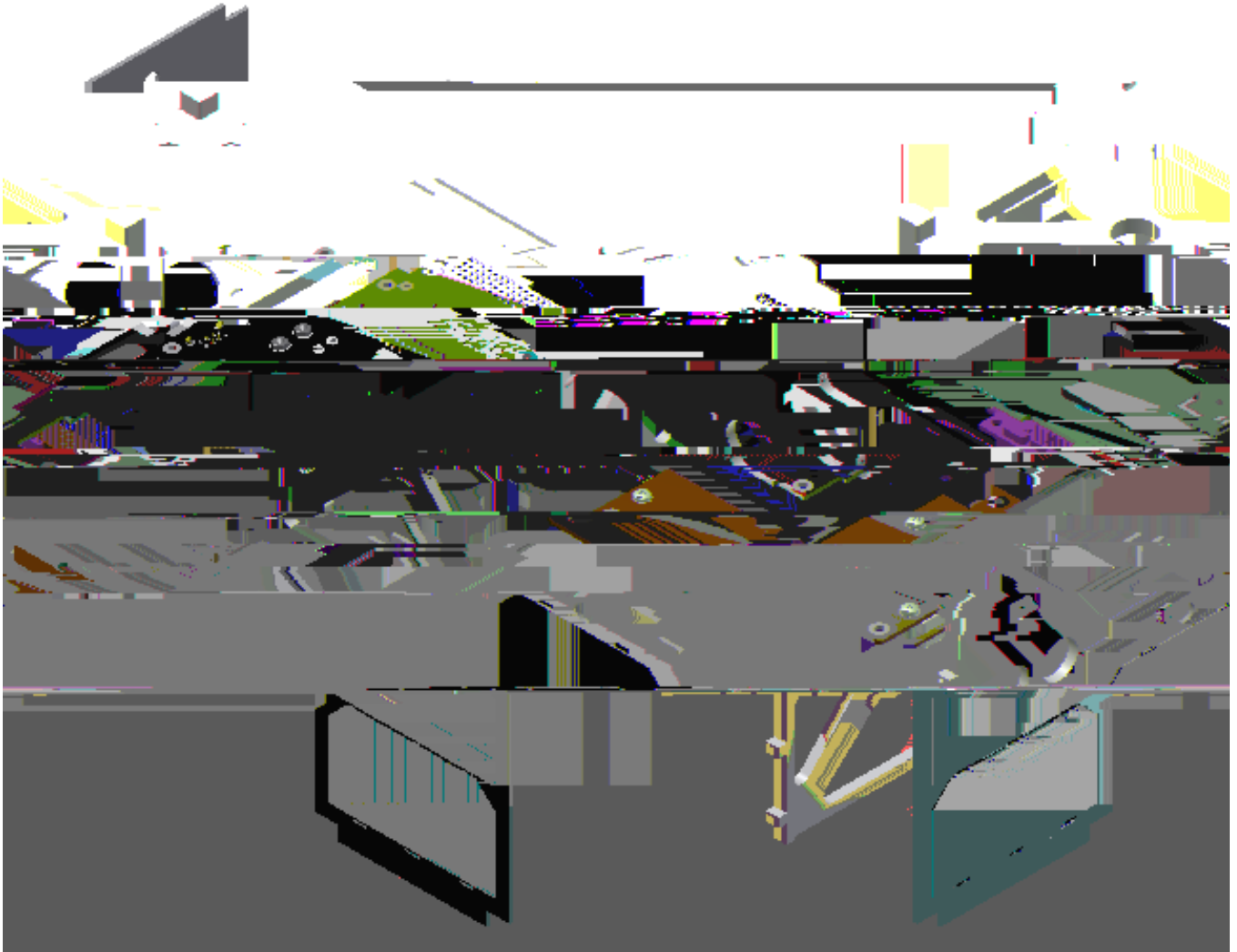


Figure #9; \$D8' rinted +u%eSat +AD Design

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Upon completion of the 3D printed +u%eSat design the satellite * as a %le to %e immediately printed.
Additionally, each of the off the shelf components including the E ' S5 Flight module, modem and B solar panels *ere printed to use as models for fit check(s and orientation. The professional grade Stratasys Elite

9.1.2 Dimensions

The +u%eSat Acceptance +hec(list <+A+=) as sho*n in Appendi7 B5 has a set of dimensional and design requirements that must %e met %y each satellite unless a deviation *aiver is su%mitted. The *idth of the #U +u%eSat must %e *ithin #""Q"t#mm and the height ##\$kCQ"t#mm. An inspection of the \$D8printed +u%eSat sho*ed the *idth to %e 99t9mm and the height ##\$k@mm. F hile the height of the rail is out of tolerance5 that could %e remedied %y reducing the dimensions in the +AD or %y simply cutting off "t\$mm from the top of each rail.

The surface finish of ABS is not applica%le as plastic has a much lo*er coefficient of friction and *ould slide more easily than aluminum.

9.1.3 Launch Loads

The launch loads are ta(en from the general launch vehicle loads as defined %y , ASA per SS ' C"@SC. This encompassed the *orse cases from all the vehicles that supply the #c' , Aye ù

E ' S card slot and the model material *as set as steel. The structure and door *ere given custom material properties using the material testing data and a tensile strength of ##kD ' at

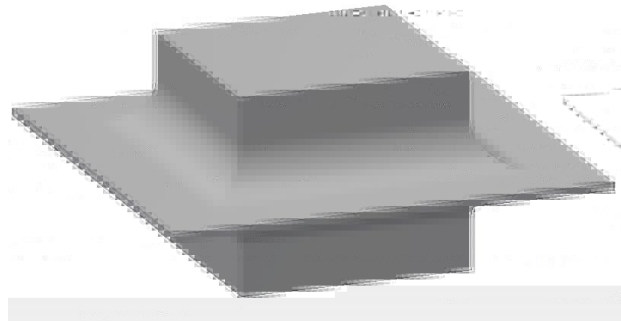


Figure !#, # (g Simulated 'ayload

A polygonal mesh *as created of the +u%eSat structure and the simulated payload, see Figure !!. The mesh included \$9!\$9 nodes and !"#ED elements. The model *as fixed on the %ottom face of each of the rails and all components *ere %onded together.

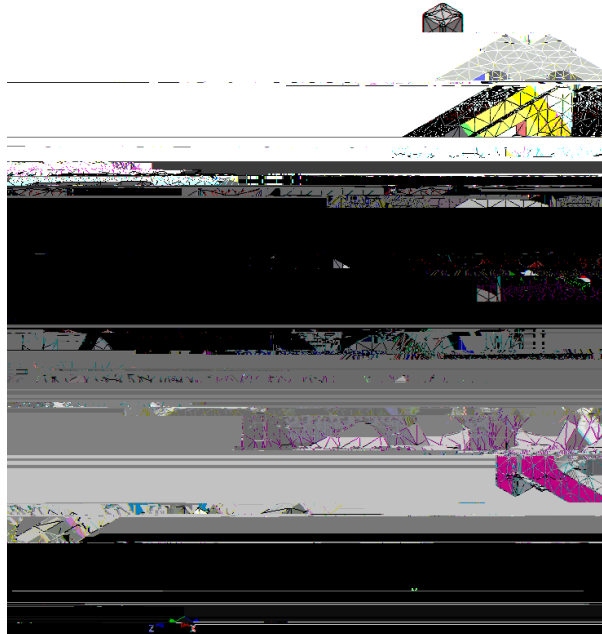


Figure 11; \$D8 'rinted +u%eSat esh

The four cases sho*ed similar results for ma7imum stresses as *ell as displacement5 see Ta%le B& The ma7imum 2on ises stresses *ere %et*een @&! X @&D 'a *hich *ere concentrated at the %ase of each rail near the constrained face5 see Figure !& 3ther areas of high stress *ere no more than \$ 'a5 *hich is %elo* the materials yield strength& a7imum displacement is "&#"C mm and is located at the top of the +u%eSat&

	a7 2on ises Stress	a7 Displacement
+ase #	@&! 'a	&#"B mm
+ase !	@&B 'a	&#"C mm

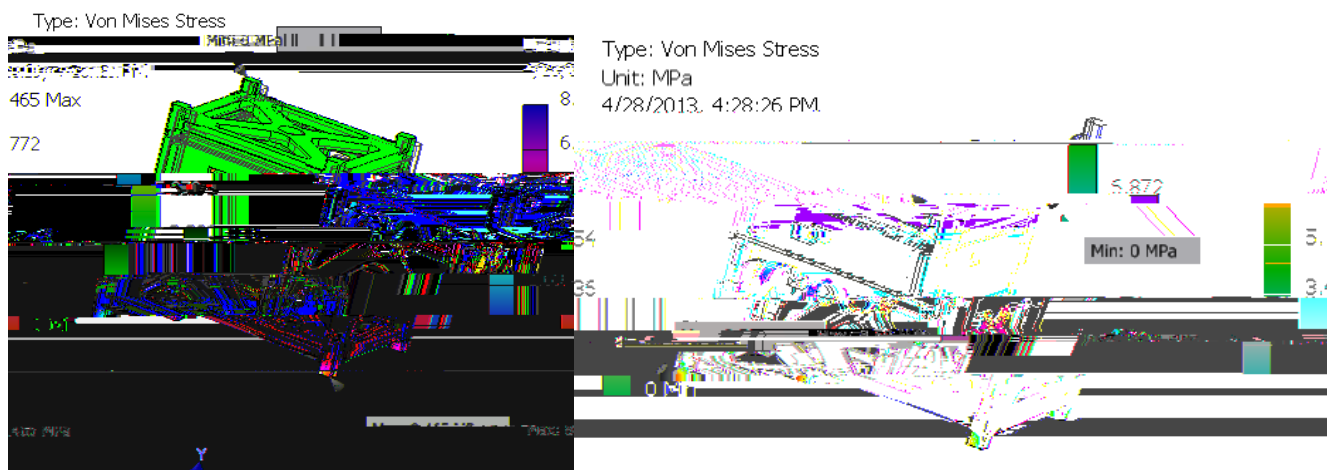
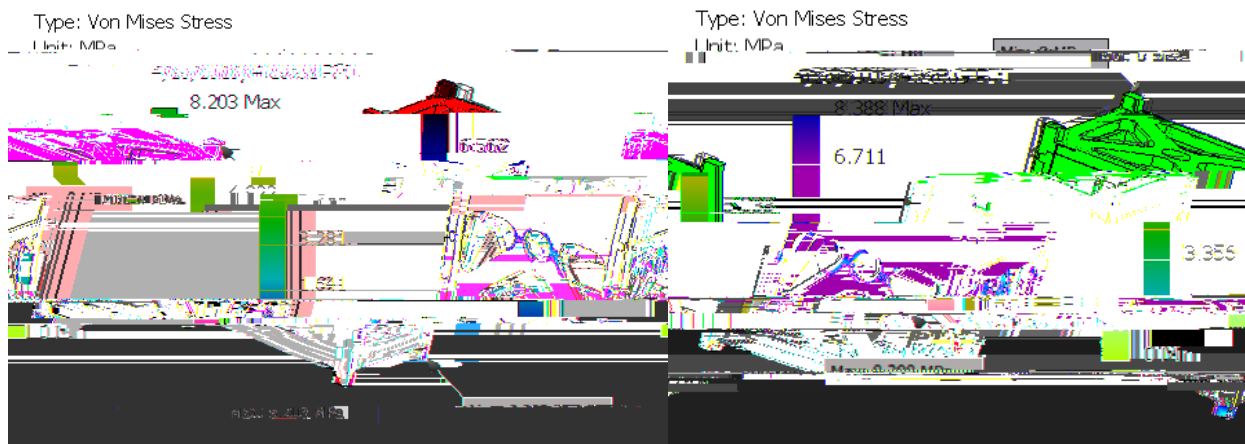


Figure 1; Von Mises Stresses Top . . . Bottom . . .

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The research and sample models printed point towards the feasibility of a functional 3D printed + user Sat. While the wall thickness would be thicker than a similar aluminum structure, the ability to customize at low manufacturing cost can offset that design constraint. ABS is a very common low end material for 3D printing.

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Figure !B; +u%eSat Specification Dra*ing

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Small Satellites for Education and Industry - 8th Space Experimentation J A/AAUSU Conference on Small Satellites August 1-8, 2011

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